



Gilberto de Barros Rodrigues Lopes

Aerodynamic Control of Flutter of Suspension Bridges

Tese de Doutorado

Thesis presented to the Postgraduate Program in Civil Engineering of the Departamento de Engenharia Civil, PUC-Rio as partial fulfillment of the requirements for the degree of Doutor em Engenharia Civil.

Advisor: Prof. Raul Rosas e Silva

Rio de Janeiro,
November 2010.



Gilberto de Barros Rodrigues Lopes

Aerodynamic Control of Flutter of Suspension Bridges

Thesis presented to the Postgraduate Program in Civil Engineering, of the Departamento de Engenharia Civil do Centro Técnico Científico da PUC-Rio, as partial fulfillment of the requirements for the degree of Doutor em Engenharia Civil.

Prof. Raul Rosas e Silva

Advisor

Departamento de Engenharia Civil - PUC-Rio

Prof. Mauro Speranza Neto

Departamento de Engenharia Mecânica - PUC-Rio

Prof. Paulo Batista Gonçalves

Departamento de Engenharia Civil - PUC-Rio

Prof. Deane Roehl

Departamento de Engenharia Civil - PUC-Rio

Prof. Uwe Starossek

Institute of Structural Analysis and Steel Structures
Hamburg University of Technology

Prof. José Luís Vital de Brito

Departamento de Engenharia Civil - Universidade de Brasília - UNB

João Luís Pascal Roehl

Consultor Externo

Prof. José Eugênio Leal

Coordinator of the Centro Técnico Científico - PUC-Rio

Rio de Janeiro, November 5th, 2010.

All rights reserved.

Gilberto de Barros Rodrigues Lopes

Graduated in Civil Engineering from Pontifícia Universidade Católica do Rio de Janeiro - PUC-Rio in December 1970. Master of Science degree in Civil Engineering also from PUC-Rio in November 1972. Masters thesis: Analysis of axisymmetric shells employing the finite element method. Thereafter studied in the Technische Universität Berlin with a Deutscher Akademischer Austauschdienst (DAAD) fellowship. Returned to Brazil in 1974 to join Société Technique pour l'Utilization de la Précontrainte (STUP). Joined Christiani-Nielsen Engenheiros e Construtores SA (CN-Brazil) in 1977. Worked for CN-Denmark in Copenhagen as a senior engineer from 1982 to 1984. Has been working since 1986 with maritime projects and shipyards, as well as concrete, prestressed concrete, steel structures and foundations as an independent structural engineer and contractor. Founded and owns CNT Consult Engenharia e Serviços Ltda and JKL Engenharia, Comércio e Construções Ltda, established in 1988 and 1987 respectively.

Bibliographic data

Lopes, Gilberto de Barros Rodrigues

Aerodynamic control of flutter of suspension bridges / Gilberto de Barros Rodrigues Lopes; advisor: Raul Rosas e Silva. — 2010.

220 f. : il.(color.) ; 30 cm

Tese (doutorado) – Pontifícia Universidade Católica do Rio de Janeiro, Departamento de Engenharia Civil, 2010.

Inclui bibliografia.

1. Engenharia Civil – Teses. 2. Aerodinâmica. 3. Aeroelasticidade. 4. Aproximações com funções racionais. 5. Controle ativo de drapejamento. 6. Superfícies de controle. 7. Pontes suspensas de grandes vãos. 8. Controle ótimo de realimentação. 9. Velocidade crítica.

I. Silva, Raul Rosas e. III. Pontifícia Universidade Católica do Rio de Janeiro. Departamento de Engenharia Civil. IV. Título.

CDD: 624

Acknowledgements

This thesis originated from my interest in instability phenomena related to the action of wind on slender structures. I want to acknowledge my admiration and appreciation to all those working in this field, whose works have influenced and instructed me. The works of the authors mentioned below, however, have been specially valuable to me:

Civil engineers Allan Larsen and Klaus Ostenfeld, of Cowi Consult, Denmark, who have first captured my imagination with the idea of wings as a means to improve the aerodynamic behaviour of very long bridges. Mr. Larsen is currently involved in the design of the Messina Bridge;

Prof. Krzysztof Wilde of the Technical University of Gdansk, Poland, for discussions concerning his articles on passive and active control of bridge deck flutter, and his advice on MATLAB programs. I am also indebted to Prof. Wilde for having provided me with a copy of a valuable FORTRAN program, written originally by civil engineer J. Masukawa and other researchers of the University of Tokyo;

Prof. Uwe Starossek, head of the Institute of Structural Analysis and Steel Structures, Hamburg University of Technology, for his advice on flutter derivatives of several bridge profiles obtained from experiments and numerical simulations;

My most sincere thanks go to my advisor and mentor, Prof. Raul Rosas e Silva for his continuous guidance and encouragement during the years of doctoral study in PUC-Rio, and for our lively discussions regarding books and authors, a favorite subject of mine.

I too would like to acknowledge my sincere gratitude to all professors I met in the Pontifícia Universidade Católica do Rio de Janeiro, during my graduate years in the 1970's, as for example the late professors Milton José de Barros Rego, (Bridges), Octavio Jost (Reinforced concrete), Raymundo de Araújo Costa, (Foundations), Antonio Carlos de Areias Neto (Steel structures), Domício Falcão Moreira (Statics), as well as all professors of my Post-graduation in the 1970's, as for example professors Nahul Benevolo and Jayme Mason. My admiration and profound respect to all professors whom I met in the last four years, during my doctoral studies, represented by professors Deane Roehl, Paulo Gonçalves and João Luís Pascal Roehl, who are present in this event as members of the Committee.

I wish to express my warm and sincere thanks to all members of this Committee for participating in this event.

I too would like to acknowledge my sincere gratitude to Prof. Mauro Speranza Neto of the Department of Mechanical Engineering for various discussions concerning the analysis and design of control systems, and Prof. Pedro Magalhães of the Department of Electrical Engineering for his brief course in Linear Systems.

I thank civil engineer Oscar Fabricio Zuleta Inch, a doctoral colleague, for his cooperation and hearty discussions on various subjects related to the present work .

I am also grateful to the staff of the Civil Engineering Department of PUC Rio, particularly to the secretary Rita de Cássia do Nascimento Leite and to Mônica de Oliveira, librarian of the CTC Sectorial Library of PUC-RJ.

I am indebted to the brazilian agencies Conselho Nacional de Pesquisas (CNPq) and Fundação CAPES for their financial support, as well as to the Pontifícia Universidade Católica do Rio de Janeiro for all the years I spent here, as a graduate student in the 70's and as a doctoral student, 40 years later. My thanks to the DAAD (Deutscher Akademischer Austauschdienst) who offered me a fellowship in 1973, in the Technische Universität Berlin, which allowed me to read several german articles on the subject matter of my thesis.

Above all, I am indebted to my parents, whom I cannot embrace anymore, and to my wife and daughters, for their love and everlasting support throughout my entire life, and specially in the last five years. This thesis is dedicated to them.

Fluvium ponte jungere.

To throw a bridge over a river.

Lançar uma ponte sobre um rio.

Lanzar un puente sobre un rio.

At slaa en bro over en flod.

Eine Brücke über einen Fluß zu schlagen.

川に橋を架ける。

Abstract

Lopes, Gilberto de Barros Rodrigues; Silva, Raul Rosas e. **Aerodynamic Control of Flutter of Suspension Bridges**. Rio de Janeiro, 2010. 220p. Doctor Thesis - Departamento de Engenharia Civil, Pontifícia Universidade Católica do Rio de Janeiro.

Long span bridges, with main spans beyond 2.000 m become highly sensitive to wind action, particularly to flutter. An active aerodynamic control method of suppressing flutter of very long span bridges is studied in this thesis. Analytical design techniques for active control of the aeroelastic system consisting of the bridge deck and two control surfaces are presented. These techniques are based on a rational approximation of the unsteady aerodynamic loads in the entire Laplace domain, which yields matrix equations of motion with constant coefficients. The first part of this thesis is dedicated to the matrix formulation of the rational functions known as "Minimum State" and to applications to aerodynamic data obtained experimentally for various types of bridge profiles. The precision of the approximations is calculated, and plots of the approximation functions compared to the available tabular data are drawn. Next, the state-space equations of motion describing the aeroelastic behaviour of a section of a bridge deck is presented. Given the dynamic data of a bridge structure (mass, rotational mass moment of inertia, natural frequencies, stiffness and damping ratios), and assuming that a geometric similitude exists between the profiles of the full-scale bridge deck and the sectional model from which the frequency dependent aerodynamic data was extracted, it is possible to calculate the critical velocity of that particular bridge. This part of the thesis shows that it is possible to build up a catalog of several profiles, characterized by frequency dependent aerodynamic data and the corresponding rational functions. The second part is dedicated to the formulation of the state-space equations of motion describing the aeroelastic behaviour of the entire system

consisting of the bridge deck and control surfaces. The resulting equation includes new aerodynamic states which model the air flow influence on the moving deck. The equation of motion is a function of the mean velocity of the incoming wind. The dependence of the equation of motion on the wind velocity motivated the application of a constant and a variable-gain feedback concept to the problem of flutter suppressing, which are presented separately. The output variable-gain approach is formulated in terms of minimizing a performance index dimensionally proportional to the sum of the work done by the rotating control surfaces and the kinetic energy of the heaving velocity. A systematic method to determine the matrix of variable control gains is shown in detail, as applied to the hypothetical case of Gibraltar bridge. Application of the variable-gain feedback concept was found to be very effective in suppressing flutter of the bridge deck. Different geometric and dynamic characteristics can be introduced in the MATLAB programs included in this work, in order to obtain the critical velocities of a bridge deck alone, a bridge deck with stationary wings and a bridge with moving wings actively controlled.

Keywords

Aerodynamics; Aeroelasticity; Approximations with rational functions; Active control of flutter; Control surfaces; Long-span suspension bridges; Optimal feedback control; Critical velocity.

Resumo

Lopes, Gilberto de Barros Rodrigues; Silva, Raul Rosas e. **Controle Aerodinâmico de Tabuleiros de Pontes com Uso de Superfícies Ativas**. Rio de Janeiro, 2010. 220p. Tese de Doutorado - Departamento de Engenharia Civil, Pontifícia Universidade Católica do Rio de Janeiro.

Pontes com vãos superiores a 2.000 m tornam-se muito sensíveis à ação do vento, particularmente ao drapejamento. Nesta tese é estudado um método para a supressão do drapejamento em pontes de grandes vãos através de um controle aerodinâmico ativo. Apresentam-se técnicas analíticas de projeto para o controle ativo do sistema aero elástico constituído pelo tabuleiro e por duas superfícies de controle. Estas técnicas são baseadas em aproximações racionais das cargas aerodinâmicas não permanentes (ou auto-excitadas) no domínio Laplaciano, no qual as equações de movimento são representadas por equações matriciais de coeficientes constantes. A primeira parte da tese é dedicada à formulação matricial das funções racionais conhecida como “Minimum State”, assim como a aplicações a dados aerodinâmicos obtidos experimentalmente para vários tipos de seções transversais de pontes. A precisão das aproximações é calculada. Desenhos dos derivativos aerodinâmicos, dados sob forma de tabelas, e das respectivas aproximações, são elaborados para fins de comparação. Em seguida, são apresentadas as equações em espaço de estado descrevendo o comportamento aeroelástico de uma seção transversal de ponte. A partir dos dados geométricos e características dinâmicas de uma determinada ponte, (massa, momento de inercia polar, frequências naturais e fatores de amortecimento), e assumindo a semelhança geométrica entre as seções transversais da ponte em verdadeira grandeza e do modelo em escala do qual os derivativos aerodinâmicos foram extraídos, é possível calcular a velocidade crítica desta ponte, utilizando os programas em linguagem MATLAB apresentados no corpo deste trabalho.

Esta parte da tese mostra ser possível construir um catálogo com vários perfis de pontes, caracterizados por derivativos aerodinâmicos variáveis em função de frequências reduzidas adimensionais, e das funções racionais correspondentes. A segunda parte é dedicada à formulação das equações de movimento em espaço de estado, descrevendo o comportamento aeroelástico do sistema “tabuleiro - superfícies de controle”. As equações resultantes são ampliadas com novos estados aerodinâmicos responsáveis pela modelagem da influência do fluxo de ar sobre o tabuleiro e sobre as superfícies de controle em movimento. As equações de movimento são função da velocidade média do vento incidente. A dependência da equação de movimento à velocidade do vento motivou a aplicação dos conceitos de realimentação de ganhos, constante e variável, ao problema da supressão do drapejamento, os quais são apresentados separadamente em dois capítulos. O enfoque de ganho variável de saída é formulado em termos de minimização de um índice de desempenho dimensionalmente proporcional à soma do trabalho realizado pelas superfícies de controle e da energia cinética proporcional à velocidade vertical do tabuleiro. Apresenta-se também em detalhe um método sistemático para determinar a matriz de controle de ganhos variável, aplicada ao caso hipotético da ponte de Gibraltar. Neste caso, o conceito de realimentação de ganhos variável mostrou-se muito efetivo em suprimir o drapejamento do tabuleiro da ponte. Diferentes características geométricas e dinâmicas de outras pontes podem ser introduzidas nos programas MATLAB apresentados no Apêndice, para obtenção da velocidade crítica nos casos de tabuleiros isolados, tabuleiros com asas estacionárias e tabuleiros com asas giratórias ativamente controladas, para supressão do drapejamento do tabuleiro.

Palavras-chave

Aerodinâmica; Aeroelasticidade; Aproximações com funções racionais; Controle ativo de drapejamento; Superfícies de controle; Pontes suspensas de grandes vãos; Controle ótimo de realimentação; Velocidade Crítica.

Contents

1. Introduction	24
1.1. Inspiration	24
1.2. Additional contributions	26
1.3. Objective	27
1.4. Sequence of presentation	28
2. Aerodynamics and aero elasticity	29
2.1. Introduction	29
2.2. Air forces acting on a vibrating flat plate	30
2.3. Notation of the unsteady forces according to Scanlan	33
2.4. Notation of the unsteady forces according to Klöppel	35
2.5. Unsteady forces, disregarding the inertia effect of the aerodynamic mass	36
2.6. Aerodynamic derivatives of various types of bridge decks	37
2.7. Methods of extraction	37
2.8. Thiesemann results	38
2.9. Buffeting forces	39
2.10. Equations of motion of the mechanical system bridge deck - wind	39
2.11. Graphs of the aerodynamic data	41
3. Rational function approximation (RFA)	43
3.1. Introduction	43
3.2. Least-squares Rational Function Approximation	44
3.3. Karpel minimum-state RFA	46
3.4. Numerical examples	48
3.5. Plots of the unsteady aerodynamic data for eight bridge profiles	55

4. Applications to single bridge decks	59
4.1.Introduction	59
4.2.Calculation of the critical velocity of a bridge deck	59
4.3.Numerical example	61
4.4.Method to determine the critical velocity of a bridge	62
5. Equation of motion of the bridge deck and wings system with active aerodynamic control	64
5.1.Formulation	64
5.2.Derivation of the equation of motion for the deck-wings system	67
5.3.The open loop system	70
6. Determination of the optimal constant output feedback gains applied to the control of a deck-wings system	74
6.1.Formulation	74
6.2.Statement of the optimization problem	77
6.3.The main result	78
6.4.Applications for aerodynamic control	80
6.5.Closed-loop systems	81
6.6.Results	84
6.7.Results of the closed loop system for $U_g = 9 \text{ ms}$, $\rho_q = 1$, $\rho_r = 5$.	87
6.8.Results of the closed loop system for $U_g = 11 \text{ ms}$, $\rho_q = 5$, $\rho_r = 30$.	91
6.9.Results of the closed loop system for $U_g = 15 \text{ ms}$, $\rho_q = 10$, $\rho_r = 300$.	96
6.10.Results of the closed loop system for $U_g = 19 \text{ m/s}$, $\rho_q = 20$, $\rho_r = 500$.	101
6.11.Conclusions	106
7. Variable-gain output feedback control	108
7.1.Introduction	108
7.2.Formulation	110
7.3.Optimization of the variable-gain output feedback control problem	114
7.4.Program fluxogram	119

7.5.Application of the variable-gains concept to the aerodynamic control of a deck wings system	121
7.6.Frequencies and damping factors of the variable gains control	124
7.7.Impulse responses of the controlled system for variable gains	127
8. Gibraltar Bridge	130
8.1.Gibraltar Bridge (deck without wings).	132
8.2.Gibraltar Bridge (deck with stationary wings).	134
8.3.Gibraltar Bridge and 3m wide wings, regulated by a variable-gain control system.	139
9. Computer programs	148
9.1.Programs related to the study of the Gibraltar bridge without wings.	148
9.2.Programs related to the study of the Gibraltar bridge with stationary wings.	152
9.3.Programs related to the study of the Gibraltar bridge with moving wings.	158
9.4.Input and Output of the FORTRAN program	170
10. Conclusions and propositions for future work	181
10.1.Conclusions	181
10.2.Propositons for future work	183
11. References	186
A. Geometric and dynamic similitude	194
A.1.Introduction	194
A.2.Example	195
B. Brazilian Code of Practice	199
B.1.Fundamentals	199
B.2.Critical speed for aerodynamic design of the Great Belt East Bridge	201
B.3.Critical speed for aerodynamic design of the Akashi Kaikyo Bridge	201
C. Values and plot of the Theodorsen function	202
D. Plots	204

D.1.Summary	204
D.2.Profile GB	205
D.3.Profile S	207
D.4.Profile M	209
D.5.Profile P	211
D.6.Profile R	213
D.7.Profile C	215
D.8.Profile TC	217
D.9.Profile G	219

List of Tables

Table 2-1 - Aerodynamic derivatives $H_i = 1,4 *$ and $A_i = 1,4 *$, considering the aerodynamic mass.....	35
Table 2-2 – Theodorsen derivatives c_{ij}' , c_{ij}'' and $H_{ij} *$, $A_{ij} *$ obtained as π -multiples of c_{ij}'	36
Table 2-3 - Aerodynamic derivatives of a flat plate, neglecting the aerodynamic mass.....	37
Table 2-4 - List of profiles examined by Thiesemann	38
Table 2-5- Unsteady aerodynamic data for a flat plate, $0.05 \leq k \leq 0.5$	41
Table 3-1 - Auxiliary variables for the calculation of the derivatives of a flat plate, valid for $0 \leq k \leq 0.05$, $0 \leq K \leq 0.10$	52
Table 3-2 - Derivatives of a flat plate, valid for $0 \leq k \leq 0.05$, $0 \leq K \leq 0.10$	53
Table 3-3 – Terms Q_{ij} for the winglets, valid for $0.005 \leq k \leq 0.05$, $0.01 \leq K \leq 0.10$, to be approximated by rational functions.....	53
Table 4-1 - Data for a 2-DOFs 2000m bridge.....	61
Table 4-2- Results of the complex eigenvalue analysis.....	63
Table 5-1 - Geometric properties of the bridge deck and wings	70
Table 5-2 - State matrix for 10.663 m/s.	71
Table 5-3 - Eigenvalues, damping and frequencies of A for 10.663 m/s	71
Table 5-4 - Diagonal matrix of the 14 eigenvalues, and eigenvectors corresponding to the eigenvalues (3,3) and (6,6).	72
Table 6-1- State Matrix $A_c = A - BKC$ for $U_{crit} = 11.910$ m/s.	87
Table 6-2- Eigenvalues, damping ratios, frequencies and eigenvectors of interest obtained from the complex eigenvalue analysis of the state matrix A_c	87
Table 6-3 - State Matrix $A_c = A - BKC$ for $U_{crit}=12.7$ m/s.....	91

Table 6-4- Eigenvalues, damping ratios, frequencies and eigenvectors of interest obtained from the complex eigenvalue analysis of the state matrix A_c .	91
Table 6-5 - State Matrix $A_c = A - BKC$ for $U_{crit} = 23.15$ m/s.	96
Table 6-6- Eigenvalues, damping ratios, frequencies and eigenvectors of interest obtained from the complex eigenvalue analysis of the state matrix A_c .	96
Table 6-7 - State Matrix for 30.67 m/s.	101
Table 6-8 - Eigenvalues, damping ratios, frequencies and eigenvectors of interest.	101
Table 7-1 - Table of eigenvalues, damping factors and frequencies of the state matrix for $U = 15.1$ m/s.	124
Table 8-1 - Comparison of Gibraltar and Akashi-Kayko Bridge deck characteristics.	131
Table 8-2 - State Matrix corresponding to $U = 47.95$ m/s.	132
Table 8-3 - Eigenvalues, damping factors and frequencies of the state matrix A for $U_{crit} = 47.95$ m/s.	133
Table 8-4 – State matrix for $A_c = A - BKC$ for $U_{crit} = 66.66$ m/s (Gibraltar Bridge with stationary wings).	136
Table 8-5 - Eigenvalues, damping factors and frequencies of the state matrix A for $U = U_{crit} = 66.66$ m/s.	136
Table 8-6 - State matrix for $A_c = A - BKC$ for $U_{crit} = 55.64$ m/s (Gibraltar Bridge with stationary wings).	138
Table 8-7 - Eigenvalues, damping factors and frequencies of the state matrix A_c for $U = 55.64$ m/s.	138
Table 8-8 - Comparison of Gibraltar and Akashi-Kayko Bridge wing characteristics.	140
Table C-1– Table with values of Bessel and Theodorsen functions.	202
Table D-1 - GB Derivatives	205
Table D-2 - Unsteady Aerodynamic Data - Experimental and approximations	206
Table D-3 - S Derivatives	207
Table D-4 - Unsteady Aerodynamic Data - Experimental and approximations	208
Table D-5 - M derivatives	209

Table D-6 - Unsteady Aerodynamic Data - Experimental and approximations .	210
Table D-7 - P Derivatives	211
Table D-8 - Unsteady Aerodynamic Data - Experimental and approximations .	212
Table D-9 - R derivatives	213
Table D-10 - Unsteady Aerodynamic Data - Experimental and approximations	214
Table D-11 - C Derivatives	215
Table D-12 - Unsteady Aerodynamic Data - Experimental and approximations	216
Table D-13 - TC derivatives	217
Table D-14 - Unsteady Aerodynamic Data - Experimental and approximations	218
Table D-15 - G derivatives	219
Table D-16 - Unsteady Aerodynamic Data - Experimental and approximations.	220

List of Figures

Figure 1-1 – Suggestions for implementation of Active Surface Systems in streamlined bridge girders, reproduced from Ostenfeld and Larsen.	24
Figure 1-2 - Section model of bridge deck and alongside wings in the small wind tunnel of the Technical University of Hamburg-Harburg	26
Figure 2-1– Force components experimented by a flat plate under wind flow. ...	31
Figure 2-2 - Unsteady aerodynamic data corresponding to Table 2-5	42
Figure 3-1 - Full expressions of Q_{11} , Q_{12} , as approximations of Q_{11} , Q_{12}	49
Figure 3-2 - Full expressions of Q_{21} , Q_{22} , as approximations of Q_{21} , Q_{22}	50
Figure 3-3 - Plots of exact and approximate values of Q_p for a flat plate using Wilde's results, valid for $0.1 < K < 1.0$ and 2 lag terms.....	51
Figure 3-4 - Plots of exact and approximate values of $Q(p)$ corresponding to the reduced frequencies $0.01 < K < 0.10$ (winglets case).....	53
Figure 3-5- Investigated profiles of typical bridge decks.....	54
Figure 3-6 - Plots of GB unsteady aerodynamic data	55
Figure 3-7 - Plots of S unsteady aerodynamic data.....	55
Figure 3-8 - Plots of M unsteady aerodynamic data	56
Figure 3-9 - Plots of P unsteady aerodynamic data.....	56
Figure 3-10 - Plots of R unsteady aerodynamic data.....	57
Figure 3-11 - Plots of C unsteady aerodynamic data.....	57
Figure 3-12 - Plots of TC unsteady aerodynamic data	58
Figure 3-13 - Plots of G unsteady aerodynamic data	58
Figure 4-1- Fluxogram 1	62
Figure 4-2 - Variation of frequencies and damping ratios versus wind velocity...	63
Figure 5-1 - Cross section of bridge deck with control surfaces	64
Figure 5-2 - Pitching and heaving frequencies versus wind velocity.....	72

Figure 5-3 - Damping ratios versus wind velocity.	73
Figure 6-1 - Variations of damping ratios and frequencies of closed-loop system with gain design for $U_g = 9$ m/s versus wind speed.....	88
Figure 6-2 - Impulse response of closed loop system with gain calculated for $U_g = 9$ m/s at $U = 9$ m/s.....	89
Figure 6-3 - Impulse response of closed-loop system with gain calculated for $U_g = 9$ m/s at $U = 11.7$ ms (near the critical 11.91m/s).....	90
Figure 6-4 -Variations of damping ratios and structural frequencies of the closed-loop system with gain design for $U_g = 11$ m/s versus wind speed.....	92
Figure 6-5 - Impulse response of closed-loop system with gain calculated for $U_g = 11$ m/s at $U = 9$ m/s.....	93
Figure 6-6 - Impulse response of the closed loop system with gain calculated for $U_g = 11$ m/s at $U = 11.5$ m/s.	94
Figure 6-7 - Impulse response of closed-loop system with gain calculated for $U_g = 11$ ms and $U = 12.7$ ms.....	95
Figure 6-8 - Variations of modal frequency ω (rd/s) of closed-loop system with gain.....	97
Figure 6-9 - Impulse response of closed loop system with gain calculated for $U_d = 15$ m/s at 9 m/s.....	98
Figure 6-10 - Impulse response of closed loop system with gain calculated for $U_g = 15$ m/s at 15 m/s.....	99
Figure 6-11 - Impulse response of closed loop system with gain calculated for $U_g = 15$ m/s at 19 m/s	100
Figure 6-12 - Variations of modal frequency ω (rd/s) and damping ratios of closed-loop system with gain design for $U_g = 19$ m/s versus wind speed.	102
Figure 6-13 - Impulse response of closed loop system with gain calculated for $U_g = 19$ m/s at 9 m/s.....	103
Figure 6-14 - Impulse response of closed loop system with gain calculated for $U_g = 19$ m/s at 12 m/s.....	104
Figure 6-15 - Impulse response of closed loop system with gain calculated for $U_g = 19$ m/s at 15 m/s.....	105

Figure 6-16 - Impulse response of closed loop system with gain calculated for $U_g=19\text{m/s}$ at 19 m/s	106
Figure 7-1 - The input is sampled and held constant over the intervals $kT, k + 1T$ by the sample-and-hold box before being applied to the system \mathcal{P}	110
Figure 7-2 - Approximation polylines.....	123
Figure 7-3 - Variation of damping factors and natural frequencies of the closed loop system with variable-gain control.	125
Figure 7-4- Plots of the rootloci from $U=9$ to 23 in steps of 1 m/s	126
Figure 7-5 - Root loci plot of all steps put together, from $U=9$ to 23 m/s	126
Figure 7-6 - Responses h/B , α , δ_1 , δ_2 of the closed-loop system to an impulse X_0 at wind velocities ranging from 9 to 21 m/s , for variable gains.....	127
Figure 7-7- Responses $d(h/B)/dt$, $d\alpha/dt$, $d\delta_1/dt$, $d\delta_2/dt$ of the closed-loop system to an impulse X_0 at wind velocities ranging from 9 to 21 m/s , for variable gains.	128
Figure 7-8 - Impulse responses of the closed loop system with static gains for $U_g = 19\text{ms}$ at 9 ms	129
Figure 8-1 –Plots of experimental data (points) and the approximating curves corresponding to rational functions ($0.38 < K < 1.13$) for the Gibraltar profile. ..	132
Figure 8-2 - Variation of damping factors and structural frequencies of the Gibraltar Bridge deck versus wind velocity	134
Figure 8-3 - Gibraltar bridge with leading and trailing control surfaces.	134
Figure 8-4 - Plots of tabular data (points) and the approximating curves corresponding to rational functions ($0.038 < K < 0.13$) for the wings 6m wide. .	135
Figure 8-5- Plots of tabular data (points) and the approximating curves corresponding to rational functions ($0.019 < K < 0.056$) for the wings 3m wide.	137
Figure 8-6 - Plots of damping ratios and structural frequencies for Gibraltar bridge with stationary wings, 3m wide.....	139
Figure 8-7 - Plots of the operating points and weights on Q , R and W (wind)..	140
Figure 8-8 -Plot of the eigenvalues of the state matrix from 1 to 76 m/s in steps of 5 m/s	144

Figure 8-9 - Plots of the eigenvalues of the state matrix from 1 to 76 m/s put together.	144
Figure 8-10 - Plots of damping factors and structural frequencies from 0 to 80 m/s.....	145
Figure 8-11 - Plots of amplitudes due to an unit impulse at $t=0$ at the operating points.....	146
Figure 8-12 - Plots of velocities due to an unit impulse at $t=0$ at the operating points.....	147
Figure 10-1- Model Reference Adaptive Control (MRAC)	184
Figure 10-2 – Linear and proposed nonlinear analysis framework	184
Figure A-1 - Cross section of the suspension bridge to be examined.....	196
Figure A-2- Wind tunnel set up showing the suspended model under wind flow.	197

Notation

$A(U)$	state-space coefficient matrix.
A_c	state-space closed-loop system matrix.
A_0, A_1, D, E, R	coefficient matrices of rational function approximations.
a_i, b_i	upper and lower limits of parameter p_i
$B, b = B/2$	bridge deck width, half width.
$B_d, B_{w1}, B_{w2}, B_u, B_{buf}$	force distribution matrices.
B_{w1}, B_{w2}	width of leading and trailing surfaces.
C	damping matrix / output matrix.
$C(k)$	Theodorsen function.
$F(k), G(k)$	real and imaginary parts of the Theodorsen function.
$c(\bullet)$	damping coefficient associated with (\bullet) coordinate.
$E(\bullet)$	expectation.
e_1, e_2	distance from control surface hinge lines to center of the deck.
F_{buf}	buffeting forces acting on deck.
F_d, F_{w1}, F_{w2}	aerodynamic forces acting on deck, leading and trailing surfaces.
H_i^*, A_i^*	flutter derivatives.
h	vertical displacement = heaving displacement.
I	identity matrix.
J	performance matrix.
K, k	reduced frequency.
K	stiffness matrix / feedback gain matrix.
K_c	coefficient matrices of variable gain.
$k(\bullet)$	stiffness coefficient associated with (\bullet) coordinate.

L, M	aerodynamic forces per unit length.
L, P	auxiliary matrices to solve Riccati's equation.
$\mathcal{L}(\bullet)$	Laplace operator.
L_i, U_i	low and upper limits of lag coefficients.
M	mass matrix.
m, I_α	mass and polar mass moment of inertia per unit length.
p	dimensionless Laplace variable.
p	vector of size q describing system operating point.
$\mathbf{Q}(p), \hat{\mathbf{Q}}(p)$	aerodynamic matrix, approximate aerodynamic matrix.
$\mathbf{q}(\bullet)$	vector of unknowns of system (\bullet)
s	Laplace variable.
$\text{tr}(\bullet)$	trace of a matrix.
U	mean wind speed.
u	control vector.
V_f	matrix of wind forces.
w_{ij}	weighing factors.
X	state-space vector
Y	output vector.
\mathbf{x}_a	vector of aerodynamic states.
$\alpha, \delta_1, \delta_2$	rotations of the deck, leading and trailing surfaces.
ε_{ij}	approximation error of RFA.
λ_i	lag coefficients.
ρ	air density.
$\rho_r, \rho_q, f(p)$	weighing functions.
Ω	transition matrix.