

Referências Bibliográficas

- ABATAN, A. O.; HOLZER, S. M. Degree of stability of geodesic domes with independent loading parameters. **Computers & Structures**, 9, 1978. 43-51.
- ALVES, R. V. **Instabilidade não-linear elástica de estruturas reticuladas espaciais**. Tese de Doutorado - PEC-COPPE/UFRJ. Rio de Janeiro. 1995.
- ANSEMS, R. B.; SCOTT, L. T. Circumtrindene: A Geodesic Dome of Molecular Dimensions. Rational Synthesis of 60 of C601. **Journal of the American Chemical Society**, 122(12), 2000. 2719-2724.
- ARIO, I.; WATSON, A. Dynamic folding analysis for multi-folding structures under impact loading. **Journal of Sound and Vibration**, 308(3), 2007. 591-598.
- BAZANT, Z.; CEDOLIN, L. **Stability of structures: elastic, inelastic, fracture and damage theories**. Oxford: UK: Oxford University Press. 1991.
- CRISFIELD, M. A. **Non-linear finite element analysis of solids and structures: advanced topics**. John Wiley & Sons, Inc. 1997.
- DE SOUZA, A. S. C. **Análise teórica e experimental de treliças espaciais**. Tese de Doutorado - Escola de Engenharia de São Carlos, USP. São Carlos. 2003.
- DEL PRADO, Z. J. G. N. **Acoplamento e interação modal na instabilidade dinâmica de cascas cilíndricas**. Tese de Doutorado - Departamento de Engenharia Civil, Pontifícia Universidade Católica do Rio de Janeiro. Rio de Janeiro. 2001.
- FAN, F.; CAO, Z.; SHEN, S. Elasto-plastic stability of single-layer reticulated shells. **Thin-Walled Structures**, 48(10), 2010. 827-836.
- GAVASSONI NETO, E. **Aplicação dos modos de vibração não lineares a modelos conceituais de estruturas offshore**. Tese de Doutorado - Departamento de Engenharia Civil, Pontifícia Universidade Católica do Rio de Janeiro. Rio de Janeiro. 2012.
- GRECO, M.; VENTURIN, W. S. Stability analysis of three-dimensional trusses. **Latin American Journal of Solids and Structures**, 3(3), 2006. 325-344.

- HRINDA, G. A. **Snap-through instability patterns in truss structures.** Nasa Langley Research Center, Hampton, Virginia, 23831. 2010.
- HUSEYIN, H. On the estimation of the stability boundary of symmetric structural systems. **International Journal of Non-Linear Mechanics**, 7, 1972. 31-50.
- KASSIMALI, A.; BIDHENDI, E. Stability of trusses under dynamic loads. **Computers & Structures**, 29(3), 1988. 381-392.
- KROTO, H. C60, fullerenes, giant fullerenes and soot. **Pure and Applied Chemistry**, 62(3), 1990. 407-415.
- KWASNIEWSKI, L. Complete equilibrium paths for Von Mises trusses. **International Journal of Non-Linear Mechanics**, 44, 2009. 19-26.
- LEE, S.; BARTHELAT, F.; HUTCHINSON, J. W.; ESPINOSA, H. D. Dynamic failure of metallic pyramidal truss core materials – experiments and modeling. **International Journal of Plasticity**, 22(11), 2006. 2118-2145.
- LEVY M.; SALVADORI M. **Why buildings fall down.** W.W. Norton & Company, New York, USA. 1987.
- LIGARO, S. S.; VALVO, P. S. Large displacement analysis of elastic pyramidal trusses. **International Journal of Solids and Structures**, 43(16), 2006. 4867-4887.
- LÓPEZ, A.; PUENTE, I.; SERNA, M. A. Numerical model and experimental tests on single-layer latticed domes with semi-rigid joints. **Computers & Structures**, 85(7), 2007. 360-374.
- MACHADO, V. L. S. S. **Bifurcações múltiplas e comportamento não-linear de sistemas dinâmicos.** Tese de Doutorado - COPPE/UFRJ. Rio de Janeiro. 1993.
- MILLON JR., S. L. **Técnicas gráficas e computacionais para a análise de oscilações não lineares e caos em sistemas estruturais suscetíveis à flambagem.** Dissertação de Mestrado - Departamento de Engenharia Civil, Pontifícia Universidade Católica do Rio de Janeiro. Rio de Janeiro. 1991.
- NAYFEH, A. H.; BALACHANDRAN, B. **Applied nonlinear dynamics. Analytical, computational and experimental methods,** New York, John Wiley & Sons, Inc. 1995.
- NAYFEH, A. H.; MOOK, D. T. **Nonlinear Oscillations,** New York, John Wiley & Sons, Inc. 1979.

OHKUBO, S.; WATADA, Y.; FUJIWAKI, T. Nonlinear analysis of truss by energy minimization. **Computers & Structures**, 27, 1987. 129-145.

ORLANDO, D. **Dinâmica não-linear, instabilidade e controle de sistemas estruturais com interação modal**. Tese de Doutorado - Departamento de Engenharia Civil, Pontifícia Universidade Católica do Rio de Janeiro. Rio de Janeiro. 2010.

PASQUETTI, E. **Métodos aproximados de solução de sistemas dinâmicos não-lineares**. Tese de Doutorado - Departamento de Engenharia Civil, Pontifícia Universidade Católica do Rio de Janeiro. Rio de Janeiro. 2008

PECKNOLD, D. A.; GHABOSSI, J.; HEALEY, T. J. Snap-through and bifurcation in a simple structure. **Journal of Engineering Mechanics**, 111(7), 1985. 909-922.

PINTO, O. C.; GONÇALVES, P. B. Active non-linear control of buckling and vibrations of a flexible buckled beam. **Chaos, Solitons & Fractals**, 14(2), 2002. 227-239.

QUEHEILLALT, D. T.; WADLEY, H. N. Pyramidal lattice truss structures with hollow trusses. **Materials Science and Engineering: A**, 397, 2005. 132-137.

SAFFARI, H.; MIRZAI, N. M.; MANSOURI, I.; BAGHERIPOUR, M. H. Efficient Numerical Method in Second-Order Inelastic Analysis of Space Trusses. **Journal of Computing in Civil Engineering**, 27(2), 2012. 129-138.

SAKA, M. P. Optimum geometry design of geodesic domes using harmony search algorithm. **Advances in Structural Engineering**, 10(6), 2007. 595-606.

SAVI, M. A.; NOGUEIRA, J. B. Nonlinear dynamics and chaos in a pseudoelastic two-bar truss. **Smart Materials and Structures**, 19(11), 2010. 1-11.

SCHIOLER, T.; PELLEGRINO, S. Space frames with multiple stable configurations. **AIAA Journal**, 45(7), 2007. 1740-1747.

SEYDEL, R. **From equilibrium to chaos: practical bifurcation and stability analysis**, New York, Elsevier Science Publishing. 1988.

SHON, S. D.; LEE, S. J.; LEE, K. G. Characteristics of bifurcation and buckling load of space truss in consideration of initial imperfection and load mode. **Journal of Zhejiang University SCIENCE A**, 14(3), 2013. 206-218.

SOLIMAN, M. S.; GONÇALVES, P. B. Chaotic behavior resulting in transient and steady state instabilities of pressure-loaded shallow spherical shells. **Journal of Sound and Vibration**, 259(3), 2003. 497-512.

TEH, L. H.; CLARKE, M. J. 1999. Tracing secondary equilibrium paths of elastic framed structures. **Journal of Engineering Mechanics**, 125(12), 1999. 1358-1364.

THOMPSON, J. M. T.; HUNT, G. W. **Elastic instability phenomena**. London, Great Britain: John Wiley and Sons. 1984.

TOKLU, Y. C. Nonlinear analysis of trusses through energy minimization. **Computers & Structures**, 82(20), 2004. 1581-1589.

WANG, B.; WU, L.; MA, L.; SUN, Y.; DU, S. Mechanical behavior of the sandwich structures with carbon fiber-reinforced pyramidal lattice truss core. **Materials & Design**, 31(5), 2010. 2659-2663.

ZOK, F. W.; WALTNER, S. A.; WEI, Z.; RATHBUN, H. J.; MCMEEKING, R. M.; EVANS, A. G. A protocol for characterizing the structural performance of metallic sandwich panels: application to pyramidal truss cores. **International Journal of Solids and Structures**, 41(22), 2004. 6249-6271.

Apêndice

Equações não lineares de movimento tendo como origem as posições de equilíbrio pré-críticas apresentadas na Tabela 1.

Para $w_1 = 0,000$

$$\begin{aligned}\bar{r}_{,\tau\tau} - \bar{r}\theta_{,\tau} + \bar{r}(\bar{r}^2 - 2w + w^2 + \delta^2) - \bar{P}_r \cos(\theta - \theta_p) &= \bar{Q} \\ \theta_{,\tau\tau} + \frac{2\bar{r}_{,\tau}}{\bar{r}}\theta_{,\tau} + \bar{P}_\theta \sin(\theta - \theta_p) &= \bar{Q} \\ w_{,\tau\tau} + w(2 + \bar{r}^2) - 3w^2 + w^3 - \bar{P}_z &= \bar{Q}\end{aligned}$$

Para $w_1 = 0,020$

$$\begin{aligned}\bar{r}_{,\tau\tau} - \bar{r}\theta_{,\tau} + \bar{r}(\bar{r}^2 - 1,96w + w^2 - 0,0396 + \delta^2) - \bar{P}_r \cos(\theta - \theta_p) &= \bar{Q} \\ \theta_{,\tau\tau} + \frac{2\bar{r}_{,\tau}}{\bar{r}}\theta_{,\tau} + \bar{P}_\theta \sin(\theta - \theta_p) &= \bar{Q} \\ w_{,\tau\tau} + w(1,8812 + \bar{r}^2) - 2,94w^2 + w^3 - \bar{P}_z &= \bar{Q}\end{aligned}$$

Para $w_1 = 0,041$

$$\begin{aligned}\bar{r}_{,\tau\tau} - \bar{r}\theta_{,\tau} + \bar{r}(\bar{r}^2 - 1,9118w + w^2 - 0,080319 + \delta^2) - \bar{P}_r \cos(\theta - \theta_p) &= \bar{Q} \\ \theta_{,\tau\tau} + \frac{2\bar{r}_{,\tau}}{\bar{r}}\theta_{,\tau} + \bar{P}_\theta \sin(\theta - \theta_p) &= \bar{Q} \\ w_{,\tau\tau} + w(1,759043 + \bar{r}^2) - 2,877w^2 + w^3 - \bar{P}_z &= \bar{Q}\end{aligned}$$

Para $w_1 = 0,064$

$$\begin{aligned}\bar{r}_{,\tau\tau} - \bar{r}\theta_{,\tau} + \bar{r}(\bar{r}^2 - 1,872w + w^2 - 0,123904 + \delta^2) - \bar{P}_r \cos(\theta - \theta_p) &= \bar{Q} \\ \theta_{,\tau\tau} + \frac{2\bar{r}_{,\tau}}{\bar{r}}\theta_{,\tau} + \bar{P}_\theta \sin(\theta - \theta_p) &= \bar{Q} \\ w_{,\tau\tau} + w(1,628288 + \bar{r}^2) - 2,808w^2 + w^3 - \bar{P}_z &= \bar{Q}\end{aligned}$$

Para $w_1 = 0,088$

$$\begin{aligned}\bar{r}_{,\tau\tau} - \bar{r}\theta_{,\tau} + \bar{r}(\bar{r}^2 - 1,824w + w^2 - 0,168256 + \delta^2) - \bar{P}_r \cos(\theta - \theta_p) &= \bar{Q} \\ \theta_{,\tau\tau} + \frac{2\bar{r}_{,\tau}}{\bar{r}}\theta_{,\tau} + \bar{P}_\theta \sin(\theta - \theta_p) &= \bar{Q} \\ w_{,\tau\tau} + w(1,495232 + \bar{r}^2) - 2,736w^2 + w^3 - \bar{P}_z &= \bar{Q}\end{aligned}$$

Para $w_1 = 0,116$

$$\begin{aligned}\bar{r}_{,\tau\tau} - \bar{r}\theta_{,\tau} + \bar{r}(\bar{r}^2 - 1,768w + w^2 - 0,218544 + \delta^2) - \bar{P}_r \cos(\theta - \theta_p) &= \bar{Q} \\ \theta_{,\tau\tau} + \frac{2\bar{r}_{,\tau}}{\bar{r}}\theta_{,\tau} + \bar{P}_\theta \sin(\theta - \theta_p) &= \bar{Q}\end{aligned}$$

$$w_{,\tau\tau} + w(1,344368 + \bar{r}^2) - 2,652w^2 + w^3 - \bar{P}_z = \bar{Q}$$

Para $w_1 = 0,146$

$$\bar{r}_{,\tau\tau} - \bar{r}\theta_{,\tau} + \bar{r}(\bar{r}^2 - 1,708w + w^2 - 0,270684 + \delta^2) - \bar{P}_r \cos(\theta - \theta_p) = \bar{Q}$$

$$\theta_{,\tau\tau} + \frac{2\bar{r}_\tau}{\bar{r}}\theta_{,\tau} + \bar{P}_\theta \sin(\theta - \theta_p) = \bar{Q}$$

$$w_{,\tau\tau} + w(1,187948 + \bar{r}^2) - 2,562w^2 + w^3 - \bar{P}_z = \bar{Q}$$

Para $w_1 = 0,181$

$$\bar{r}_{,\tau\tau} - \bar{r}\theta_{,\tau} + \bar{r}(\bar{r}^2 - 1,638w + w^2 - 0,329239 + \delta^2) - \bar{P}_r \cos(\theta - \theta_p) = \bar{Q}$$

$$\theta_{,\tau\tau} + \frac{2\bar{r}_\tau}{\bar{r}}\theta_{,\tau} + \bar{P}_\theta \sin(\theta - \theta_p) = \bar{Q}$$

$$w_{,\tau\tau} + w(1,012283 + \bar{r}^2) - 2,457w^2 + w^3 - \bar{P}_z = \bar{Q}$$

Para $w_1 = 0,223$

$$\bar{r}_{,\tau\tau} - \bar{r}\theta_{,\tau} + \bar{r}(\bar{r}^2 - 1,554w + w^2 - 0,396271 + \delta^2) - \bar{P}_r \cos(\theta - \theta_p) = \bar{Q}$$

$$\theta_{,\tau\tau} + \frac{2\bar{r}_\tau}{\bar{r}}\theta_{,\tau} + \bar{P}_\theta \sin(\theta - \theta_p) = \bar{Q}$$

$$w_{,\tau\tau} + w(0,811187 + \bar{r}^2) - 2,331w^2 + w^3 - \bar{P}_z = \bar{Q}$$

Para $w_1 = 0,280$

$$\bar{r}_{,\tau\tau} - \bar{r}\theta_{,\tau} + \bar{r}(\bar{r}^2 - 1,44w + w^2 - 0,4816 + \delta^2) - \bar{P}_r \cos(\theta - \theta_p) = \bar{Q}$$

$$\theta_{,\tau\tau} + \frac{2\bar{r}_\tau}{\bar{r}}\theta_{,\tau} + \bar{P}_\theta \sin(\theta - \theta_p) = \bar{Q}$$

$$w_{,\tau\tau} + w(0,5552 + \bar{r}^2) - 2,16w^2 + w^3 - \bar{P}_z = \bar{Q}$$

Para $w_1 = 0,423$

$$\bar{r}_{,\tau\tau} - \bar{r}\theta_{,\tau} + \bar{r}(\bar{r}^2 - 1,154w + w^2 - 0,667071 + \delta^2) - \bar{P}_r \cos(\theta - \theta_p) = \bar{Q}$$

$$\theta_{,\tau\tau} + \frac{2\bar{r}_\tau}{\bar{r}}\theta_{,\tau} + \bar{P}_\theta \sin(\theta - \theta_p) = \bar{Q}$$

$$w_{,\tau\tau} + w(-0,001213 + \bar{r}^2) - 1,731w^2 + w^3 - \bar{P}_z = \bar{Q}$$