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Anexo I: Dados Técnicos do Sensor de Pressão Kistler tipo 2852A

SCP Slim for Engine Indication, Signal Conditioning Platform with optional PiezoSmart®
Types 2852A..., 4665Y51, 5064A...Y51, 5269Y51

KISTLER

measure. analyze. innovate.

Technical Data SCP Slim Type 2852A...

Chassis		
Module cards	max.	2
Channels per rack		4
with rack combination	max.	16
Power supply		
Standard (single module)	VDC	10 ... 36
Standard (cascading up to 4 modules)		11 ... 36
With external power supply	VAC	100 ... 240, ±10 %
Power consumption max.	W	20
Inrush current (Main und 3 Extension)	A	≈13
Degree of protection	IP	40
Fuse		8A slow-blow (SPT)
Operating temperature range ¹⁾	°C	0 ... 50
Min. / max. temperature range ¹⁾	°C	-40/50
Dimensions Type 2852A...		
Height	HE (mm)	1 (41)
Width	mm	220
Depth	mm	230
Weight	kg	≈1,6
Software		
	Graphical User Interface (GUI)	
	COM components for	
	Microsoft Windows, 2000, XP	

¹⁾ non condensing

Connections

Analog-Output/Interface (integrated)		
Analog outputs		4
Voltage	V	0 ... ±10
Current (per channel)	mA	0 ... ±2
Error	%	<±0,1
Trigger output (optocouplers)		
High	V	>2,4
Low	V	<0,8
Pull-up on +5 V RS	kΩ	10
Connection	Type	D-Sub 37 pin neg.

Interface		
Interface	Type	RS-232C
Connexion	Type	D-Sub 9 pin neg.

Digital I/O

Digital I/O Trigger/ Operate		
Input Optokoppler	–	Trigger via Optokoppler on analog output
High	V	3 ... 30
Low	V	<2
Current input High	mA	2 ... 29
Pull-up on +24 V (connectable)	kΩ	10
Pull-down on DGND (connectable)	kΩ	1
Connection	Type	D-Sub 9 pin neg.
Digital output DOUTA1 ... B4		
	–	isolated solid with Foto/Mos Relais
Current load (continuous)	mA	<100
Voltage (continuous)	V	<±42
Voltage for external devices	V	24
Current draw max.	mA	50
Connection	Type	D-Sub 15 pin neg.

Anexo II: IPOD 8427

Controlador desenhado para todos os tipos de injetores de bobina (solenóide) este equipamento oferece diferentes modos de controle de cada corrente, tensão ou tempo utilizado no modo de comando dentre suas principais características:

- IPOD 8427 apresenta seis configurações de condução adaptados para seu uso com diferentes injetores comerciais;
- Cada IPOD 8427 só pode ter controle sobre um injetor (conexão X6 EV);
- O IPOD 8427 é utilizado através do software XIPOD;

Para poder utilizar mais de um IPOD a comunicação deve ser feita através de uma ligação do RS485 ou de um conversor do tipo RS232/RS485 em este caso a comunicação com múltiplos IPODs é possível.

O software XIPOD pode controlar múltiplos IPOD's iguais (só injetores de bobina).

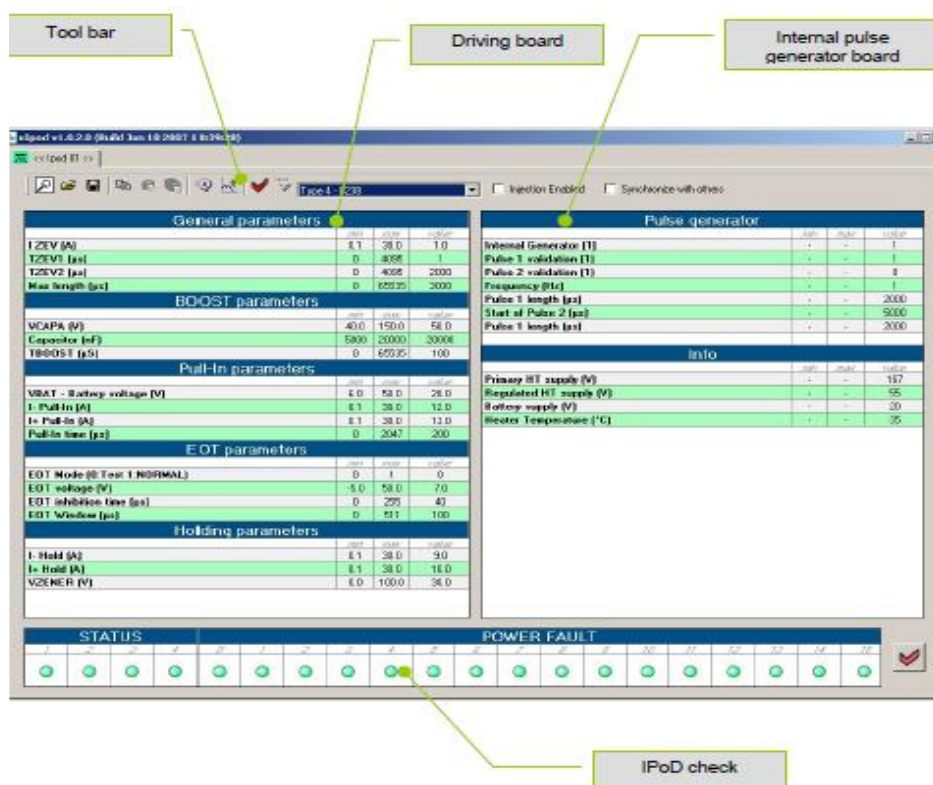


Figura A1 - Tela do software XIPOD.

Anexo III: High Pressure Regulator (HPR) 8244

O sistema HPR permite a regulação de alta pressão dentro dos sistemas de injeção diesel (common rail). Em função da alta pressão do sistema, um ou dois atuadores podem ser utilizados para regular a alta pressão. O comando é adaptado a cada tipo de sistema em função de:

- Número e do modo de funcionamento dos atuadores.
- Sinais provenientes da bomba.

O HPR instalado no LEV possui a seguinte configuração:

- Quadro de alimentação EFS 1712.
- Quadro de controle dos atuadores EFS 1522 (dois).
- Quadro do CPU. Unidade Central do regulador de alta pressão EFS 1521.
- Quadro de isolamento e adaptação dos sinais logicas de entrada e saída EFS 1526.
- Quadro de alimentação do captador de pressão EFS 1520.
- O HPR instalado no LEV possui dois quadros do tipo EFS1522 cada um deles configurado para o controle de atuadores para Diesel (X4) ou Gasolina (X5).

O software que é utilizado para configurar o HPR é o WINHPR com ele podem ser selecionados os parâmetros do atuador desejado (entre os quatro configurações para cada sistema). O software detecta automaticamente os portos de comunicação presentes e não utilizados.



Figura A2 - Tela do software WINHPR

Anexo IV: Propriedades Termofísicas

Tabela IV – Propriedades termofísicas do ar, diesel e etanol (20°C e 1atm)

Propriedades	Unidades	Ar	Diesel	Etanol
Massa Molar	kg/kmol	28,97	170	46,07
Massa Especifica a 20°C	kg/m ³	1,2	820-850	789
Calor especifico a Volume cte, cp	kJ/kg.K	1	2,688	2,39
Calor especifico a Pressão cte, cp	kJ/kg.K	0,718	2,737	-
Relação de calores específicos	-	1,4	1,018	26,7
Condutividade Térmica	W/m.K	26,24	0,03134	-
Calor latente de vaporização	kJ/kg	-	-	903
Constante de gás ou vapor ideal	kJ/kg.K	0,287	-	-
Viscosidade absoluta	Cst	0,01846x10 ⁻³	3,71	1,78
Relação ideal ar-combustível	kg/kg	-	15,14/1	9,07
Limites flamabilidade vol.	%	-	0,5-0,7	4,3-19
Poder Calorifico inferior	kJ/kg	-	42,45	26,75

Anexo V: Análise de incertezas experimentais

Nos resultados finais de trabalhos experimentais, existem erros provenientes de fatores que influenciam na precisão de medição, tais como: incerteza do instrumento de medição, metodologia empregada e erros aleatórios. Para atenuar os efeitos desses erros, costuma-se repetir a medida várias vezes e efetuar um tratamento estatístico. O emprego de um método estatístico em um estudo científico aplica-se quando a variabilidade, complexidade ou parcial desconhecimento das origens do fenômeno comprometem a confiabilidade dos resultados. O resultado obtido pelas técnicas estatísticas permite alcançar uma série de comportamentos gerais frente a casos acidentais ou isolados, com os quais se fabrica um modelo. No Brasil, o INMETRO (Instituto Nacional de Metrologia, Normalização e Qualidade Industrial) publicou o “Vocabulário Internacional de Termos Fundamentais e Gerais de Metrologia” (1995) que está em consonância com o ISO 4006 “The International Standardisation Organization” e define o termo Incerteza como “Parâmetro, associado ao resultado de uma medição. Que caracteriza a dispersão dos valores que poderiam ser razoavelmente atribuídos ao mensurado”. Em outras palavras, Incerteza de Medição (Uncertainty of Measurement) é a metade da faixa dentro do qual o valor verdadeiro (ou convencional) é esperado acontecer com uma determinada probabilidade.

Taylor e Kuyatt (1993) descrevem que a propagação das incertezas experimentais da medida de variáveis independentes ($x_1, x_2, \dots, x_n$), pode ser estimada da seguinte média pitagórica

$$I_Y = \frac{\delta I_Y}{I_Y} = \pm \left\{ \left(\frac{x_1}{Y} \frac{\partial}{\partial x_1} \right)^2 + \left(\frac{x_2}{Y} \frac{\partial}{\partial x_2} \right)^2 + \dots + \left(\frac{x_n}{Y} \frac{\partial}{\partial x_n} \right)^2 \right\}^{\frac{1}{2}} \quad (A-1)$$

Como neste trabalho foram obtidos resultados dependentes de medições individuais, decidiu-se explicitar a propagação das incertezas de medição, ou seja, a incerteza do resultado consiste no conjunto de incertezas de outras variáveis independentes relacionadas com o resultado final.

A tabela A-1 apresenta a incerteza padronizada dos principais medidores utilizados na experiência:

Parâmetros Avaliados	Unidade	Incerteza
Massa de óleo diesel	g	0,1 g
Massa de etanol hidratado	g	0,1 g
Pressão*	Bar	$\pm 0,1\%$
Resolução da MCR	mm	0,05 mm

*A classe de precisão de um sensor KISTLER é determinada pelo valor máximo de grandezas de influência especificados (em percentagem), no entanto, a precisão não corresponde ao esquema de classificação de acordo com as diretrizes EN ISO 376 ou DIN 51309.