

Internal Research Reports

ISSN

Number 9 | August 2010

On Implementable Transfer Matrices

Pedro M. G. Ferreira



Internal Research Reports

Number 9 | August 2010

On Implementable Transfer Matrices

Pedro M. G. Ferreira

CREDITS

Publisher:

MAXWELL / LAMBDA-DEE

Sistema Maxwell / Laboratório de Automação de Museus, Bibliotecas Digitais e Arquivos

http://www.maxwell.vrac.puc-rio.br/

Organizers:

Alexandre Street de Aguiar Delberis Araújo Lima

Cover:

Ana Cristina Costa Ribeiro

© 1990 IEEE. Reprinted, with permission, from IEEE TRANSACTIONS ON AUTOMATIC CONTROL, VOL. 35, NO. 3, MARCH 1990.

This material is posted here with permission of the IEEE. Such permission of the IEEE does not in any way imply IEEE endorsement of any of Pontificia Universidade Catolica do Rio de Janeiro's. Internal or personal use of this material is permitted. However, permission to reprint/republish this material for advertising or promotional purposes or for creating new collective works for resale or redistribution must be obtained from the IEEE by writing to pubs-permissions@ieee.org.

By choosing to view this document, you agree to all provisions of the copyrightlaws protecting it.

On Implementable Transfer Matrices

PEDRO M. G. FERREIRA

Abstract—A straightforward proof is given of the sufficient condition for implementable transfer matrices. A similar result is obtained also when the controlled output is not accessible for feedback.

I. INTRODUCTION

In [1] the interesting and useful definition of implementable transfer matrices was introduced and explored. The definition goes as follows.

Let $P \in M(R(s))$ be a proper transfer matrix, with input u and output y. Let r be an exogenous signal. Then the transfer matrix H_{yr} between y and r is implementable if there exists a configuration and compensators so that the resulting system implements H_{yr} under the following conditions.

- 1) All forward paths from r to y pass through the plant P.
- The closed-loop transfer matrix of every possible input-output pair is well defined, proper, and stable.
 - All compensators have proper transfer matrices.
 Remarks:
- i) The definition is phrased in a slightly different, but equivalent way in [1].

Manuscript received December 12, 1988; revised March 29, 1989. This work was supported by MCT and CNPq.

The author is with the Pontificia Universidade Católica, Rio de Janiero, Brazil. IEEE Log Number 8933233.

ii) The inputs referred to in condition 2) above are exogenous inputs entering the configuration, including r. The outputs are y and any signal between plant and compensators and between the compensators themselves.

II. FEEDBACK OF THE CONTROLLED OUTPUT

The following result, given in [1], is proved here in a straightforward way, using factorizations over proper and stable rational matrices.

Theorem 1: Assume that y is accessible for feedback. Then H_{yy} is implementable if and only if it is proper and stable and can be decomposed as $H_{rr} = PT$, where T is proper and stable.

Proof: As pointed out by [1], the necessity follows directly from conditions 1) and 2) above. Indeed, from condition 1) it follows that $H_{sr} = PT$, for some $T \in M(R(s))$. From condition 2) it follows that T is proper and stable because T is the transfer matrix between u and r.

(Sufficiency): Let S denote the set (a Euclidean domain) of proper and stable rational functions. Let $N, D \in M(S)$, right coprime and such

$$P = ND^{-1}$$

$$\therefore H_{yr} = ND^{-1}T.$$

Now $H_{yr} \in M(S)$ implies, in view of the coprimeness of N and D (see [4]), $D^{-1}T \in M(S)$. Hence, $H_{yr} = NQ$, for some $Q \in M(S)$. Next choose the following compensator with two degrees of freedom [4, sect. 5.6]:

$$u = \tilde{D}_{\epsilon}^{-1}[Q| - \tilde{N}_{\epsilon}] \begin{bmatrix} r \\ y \end{bmatrix}$$

The lemma in [4, p. 114] guarantees the existence of $D_c^{-1}N_c$ which stabilizes the loop and which is proper.

Moreover, with such a compensator we obtain indeed [4, sect. 5.6] $H_{yy} = NQ$, with conditions 1)-3) satisfied.

Some remarks are in order.

- 1) In [1] the theorem is stated formally only as a necessary condition without the assumption on the accessibility of y for feedback, an assumption which is not used, as a matter of fact, in the proof of the necessity of the theorem. Then [1] gives a proof of the sufficiency of the theorem without mentioning the above assumption but in fact using it.
- "H_y, proper and stable" is obviously included in condition 2). so it could be omitted if the theorem were stated only as a necessary condition.
- 3) The proof would be the same if the linear systems were defined in the more general algebraic structure (g, h, i, j), which encompasses, as a special case, transfer matrices which are rational and proper: see, e.g., [5] and the references therein. The only additional assumption would be that the elements of P are in the Jacobson radical of g (see 15, lemma 1.14]). This assumption corresponds, for lumped-parameter systems, to strictly proper transfer matrices.
- 4) The proof of the sufficiency above cannot be carried out with polynomial factorizations. To see this, let N_0 and D_0 be right coprime polynomial matrices with D_0^{-1} proper and such that $P = N_0 D_0^{-1}$. Then, using a reasoning which is slightly more involved than the one used above, it is easy to see that there exists Q_0 , proper and stable and such that $ii_{rr} = N_n Q_0$.

Let D_q and N_q be left coprime polynomial matrices such that $Q_0 =$ Do Ng. Hence,

$$H_{yr} = N_0 \tilde{D}_o^{-1} \tilde{N}_g. \tag{1}$$

Let C_0 be a compensator with two degrees of freedom, i.e., $C_0 =$ $\tilde{D}_1^{-1}[\tilde{N}_1 \ \tilde{N}_2]$, a left coprime factorization over polynomial matrices. It is straightforward to see that $H_{yy} = N_0(\tilde{D}_1D_0 + \tilde{N}_2N_0)^{-1}\tilde{N}_1$. In view of (1), choose \tilde{D}_1 , \tilde{N}_1 , and \tilde{N}_2 such that $\tilde{D}_q = \tilde{D}_1 D_0 + \tilde{N}_2 N_0$ and $N_1 = N_q$. Are we done? No, we are not, because there is no guarantee that Co is proper. Moreover, let an exogenous signal wenter the loop at the plant's input. It is easy to see that $H_{\mu\nu}$ and $H_{\nu\nu}$ are $D_0(\bar{D}_1D_0 + \bar{N}_2N_0)^{-1}\bar{D}_1$ and $N_0(\bar{D}_1D_0 + \bar{N}_2N_0)^{-1}\bar{D}_1$, respectively. It is clear that there is no guarantee that these matrices are proper with the above choices of D_1 and N_2 . Again we reach the same conclusion if we consider the transfer matrices with respect to an exogenous signal entering the loop at the plant's output.

In [1] Chen and Zhang proved the sufficiency of the theorem using polynomial factorizations. In order to take care of the properness problem shown above, their proof is much less straightforward. The bonus is that their constructive proof is more ready to be implemented as an algorithm for actual design.

III. FEEDBACK OF THE MEASURED OUTPUT

In many practical situations the controlled output (y) is not accessible for feedback. Assume then that y is not accessible for feedback, but ym is. Let $y_m = P_m u$. Define the right coprime factorization over S

$$\begin{bmatrix} P \\ P_m \end{bmatrix} = \begin{bmatrix} \overline{N} \\ N_m \end{bmatrix} D^{-1}.$$

Implement a two-parameter compensator

$$u = \tilde{D}_c^{-1}[Q| - \tilde{N}_c] \begin{bmatrix} r \\ y_m \end{bmatrix}$$

with $\tilde{D}c$, \tilde{N}_c , and $Q \in M(S)$ and $\tilde{D}_c^{-1}\tilde{N}_c$ a stabilizer of the loop. It is well known [5] that there exists such a loop stabilizer if and only if N_m and D are right coprime. If this is the case, it is easy to prove (see [5]) that $H_{rr} = \bar{N}Q$.

Now let $H_{yr} = PT = \overline{N}D^{-1}T$, $T \in M(S)$. But $H_{yr} \in M(S)$ implies $D^{-1}T \in M(S)$ if \overline{N} and D are right coprime. So we have the following

Theorem 2: Let y_m be the accessible output for feedback. Assume that both (N_m, D) and (\overline{N}, D) are right coprime pairs. Then H_p , is implementable if and only if it is proper and stable and can be decomposed as $H_{yy} = PT$, where T is proper and stable.

REFERENCES

- [1] C. T. Chen and S.-Y. Zhang, "Various implementations of implementable transfer matrices," IEEE Trans. Automat. Contr., vol. AC-30, pp. 1115-1118, Nov.
- [2] C. T. Chen, "Introduction to the linear algebraic method for control system design," IEEE Contr. Syst. Mag., vol. 7, pp. 36-42, Oct. 1987,
- M. Horowitz, Synthesis of Feedback Systems. New York: Academic, 1963. M. Vidyasagar, Control System Synthesis: A Factorization Approach. Cam-
- bridge, MA: M.I.T. Press, 1985.
- C. A. Desoer and A. N. Gündes, "Algebraic theory of linear time-invariant feedback systems with two-input two-output plant and compensator," Int. J. Contr., vol. 47, pp. 33-51, Jan. 1988.